

NEEDS: For the City Council to confirm the site for, and primary building characteristics of, a new Senior/Veteran's Center.

FACTS: 1. Measure D-98 authorized $\$ 1,500,000$ for a new "Senior/Veteran's Center."
2. A number of sites and facility alternatives for a Senior/Veteran's Center have been considered over the past twelve months.
3. Recently, the Council directed evaluation of an option to construct a new facility on City owned property in the vicinity of Sherwood \& Oak Creek Parks.
4. The City owns nearly 27 acres of open space in and around Sherwood and Oak Creek Parks.
5. Early in the evaluation, Council determined it prudent to "master plan" the 27 acre site to ensure optimal placement of a Senior/Veteran's Center, as well as longterm park improvement options.
6. Mr. Fred Sweeney, of Phillips, Metsch, Sweeney \& Moore, was retained to assist in the evaluation.
7. The proposed Master Plan includes a Senior Center \& Veteran's War Memorial Building, two full size softball fields (also suitable for little league play), a full size soccer field, a second soccer field sized to accommodate regulation football, a future youth center, basketball and volleyball courts, new play structures and picnic areas, and space for an aquatic center (Exhibits A \& B).
8. Optimal and safe use of available open space for the Senior Center \& Veteran's War Memorial Building, and redesigned and enlarged softball and soccer fields, indicates a need to close Scott Street from Via Ramona to Creston Road.
9. A traffic study has been completed to determine the traffic impacts of such a closure (Exhibit C). Traffic diverted from Scott Street can be safely handled by other area traffic ways including Commerce Way to Sherwood Road, Via Ramona to Creston Road via Santa Ynez, and Driftwood to Creston Road via Cedarwood.

## ANALYSIS \&

CONCLUSION: The Sherwood \& Oak Creek Parks Master Plan would provide a blueprint for the long-term improvement of a major park facility. The resulting 27 acre park would offer attractions for users of all ages. The first phase of the Master Plan can be
accomplished within two years with the development and construction of a Senior Center \& Veteran's War Memorial Building.

As proposed, the Senior Center \& Veteran's War Memorial Building site allows easy access from Creston Road via public transportation, the existing Sherwood Park parking lot, and the existing (and planned for expansion) Cedarwood Street Oak Creek Park parking lot. For users of the future Senior Center \& Veteran's War Memorial Building, ready and safe access from the Sherwood Park lot, and to other Master Plan Park attractions, would be facilitated by the partial closure of Scott Street.

POLICY
REFERENCE: Measure D-98; Fiscal Year 1999-2002 City Financial Plan.
FISCAL
IMPACT: $\quad \$ 1,500,000$ for design and construction of a "Senior/Veteran's Center" from Measure D-98 bond proceeds.

OPTIONS: A. Authorize the Design of a New Senior Center \& Veteran's War Memorial Building by Taking the Following Actions:

- Approve the Site \& Building Concept as in Exhibits A \& B;
- Endorse the Closure of Scott Street from Via Ramona west to Creston Road;
- Endorse the Sherwood/Oak Creek Park Master Plan; and
- Direct Building Architect Selection.
B. Modify Site, Building Concept, Street Closure and/or Master Plan Features and Then Approve (as above).
C. Amend, Modify or Reject Options Above.

[^0]John McCarthy
City of Paso Robles
1030 Spring Street
P.O. Box 307

Paso Robles, CA 93447-307

## TRAFFIC \& CIRCULATION STUDY <br> FOR THE SCOTT STREET CLOSURE PROJECT, CITY OF PASO ROBLES


#### Abstract

Associated Transportation Engineers (ATE) has prepared the following traffic and circulation study for the Scott Street Closure Project. The traffic study presents existing traffic conditions within the area based on collection of traffic counts and patterns. The traffic effects of the closure are defined based on the existing volumes and patterns, including quantifying traffic volume diversions to alternative routes. The ability of area roadways to accommodate the traffic diversions was then determined.


## PROJECT DESCRIPTION

The project would close the first block of Scott Street between Creston Road and Via Ramona. Scott Street is a 2-lane east-west collector road that extends from Creston Road on the west to Eastview Place on the east (just east of Airport Road). Sherwood Park, a park developed with recreational facilities such as ball fields and play equipment, is located on the north side of the road within the first block. Oak Creek Park, a passive park with picnic facilities, is located on the south side of the road within the first block. The first block of Scott Street has curb, gutter and sidewalk on the north side of the road fronting Sherwood Park, and a paved shoulder on the south side of the road fronting Oak Creek Park. The pavement width is 36 feet within the first block, with a 22 -foot westbound lane and an 11foot eastbound lane + a 3 -foot shoulder. East of Commerce Way the roadway winds through a residential area. This segment is fully constructed to collector road standards, containing a 44-foot curb-to-curb width. Sidewalks are provided on both sides of the street in the residential area.

## AREA STREET NETWORK

The street network potentially affected by the closure is made up of arterials, collectors and local streets, as illustrated in Figure 1 (attached). The following text provides a brief discussion of key components of the area street network.

Niblick Road-Sherwood Road, located north of Scott Street, is an east-west arterial roadway that extends east and west of Creston Road. West of Creston Road, the roadway is named Niblick Road and extends across the Salinas River. East of Creston Road, the roadway is named Sherwood Road and extends to Fontana Road, which turns southerly and extends to Linne Road. Linne extends easterly from this point.

Creston Road is a north-south 4-lane arterial in the study area. The Creston Road/Niblick Road-Sherwood Road intersection is controlled by traffic signals, the Creston Road/Santa Ynez intersection is controlled by an all-way stop, the Creston Road/Scott Street intersection is controlled by a 1 -way stop (Scott Street stopped), and the Creston Road/Cedarwood intersection is controlled by traffic signals.

Santa Ynez Avenue is a 2 -lane local street that extends easterly from Creston Road to Camino Lobo. This roadway serves residential uses on the north and east, and Sherwood Park on the south.

Via Ramona and Camino Lobo are 2-lane local streets that extend between Santa Bella and Scott Street, serving single family residences. Both of these streets are 40 feet in width with curb, gutter and sidewalk.

Commerce Way is an industrial streets that runs north-south between Scott Street and Sherwood Road. Commerce Way contains curb, gutter and sidewalk, and is 85 feet in width. The street is heavily parked during working hours by employees of the adjacent businesses as well as some semi-tractor trucks.

Cedarwood Drive is a 2 -lane local street that extends east of Creston Road to Redwood Drive. This roadway serves Oak Creek Park and commercial uses near Creston Road, and the residential neighborhood to the east of the park. The Creston Road/Cedarwood Drive intersection is controlled by traffic signals.

Airport Road is a 2-lane collector road that runs north-south between Meadowlark Road and Linne Road.

Meadowlark Lane is a 2 -lane collector road that extends east of Creston Road to beyond Airport Road. The Creston Road/Meadowlark Road intersection is controlled by an allway stop.

## TRAFFIC PATTERNS AND AREA OF INFLUENCE

Traffic volumes and patterns were collected for the first block of Scott Street to determine traffic that would be affected if the street were closed. 3,050 average daily trips (ADT) currently use the first block of Scott Street. Traffic volumes are fairly consistent throughout the day between 7:00 A.M. and 6:00 P.M. The hourly volumes range between 80 and 135 vehicles eastbound and 65 to 140 vehicles westbound during the 7:00 A.M. to 6:00 P.M. period. The traffic patterns indicate that about $70 \%$ of the traffic is oriented to the north on Creston and $30 \%$ to the south on Creston. Based on the volumes and patterns, the "area of influence" was determined to be primarily the residential uses east of Commerce Way; and to a lesser degree the southern portions of Via Ramona, Camino Lobo and Commerce Way, and the northern portion of the Driftwood Drive neighborhood. This area of influence is depicted on Figure 2.

## EXISTING VOLUMES AND LEVELS OF SERVICE

Existing ADT volumes were collected for the key area streets that would be affected by traffic diversions resulting from the proposed street closures. A.M. and P.M. peak hour turning volumes were also collected at the key intersections that would be affected. Figure 3 shows the existing volumes and Tables 1 and 2 show the roadway and intersection levels of service. LOS A through LOS F are used to rate roadway and intersection operations, with LOS A indicating very good operations and LOS F indicating poor operations with heavy congestion.

Table 1
Existing Roadway Operations

| Roadway | Type | Volume | LOS |
| :--- | :---: | ---: | :---: |
| Scott Street w/o Creston Road | Collector | 3,050 ADT | LOS A-B |
| Creston Road n/o Sherwood Road | Arterial | 14,500 ADT | LOS A-B |
| Creston Road s/o Sherwood Road | Arterial | 13,500 ADT | LOS A-B |
| Sherwood Road e/o Creston Road | Arterial | 8,500 ADT | LOS A-B |
| Niblick Road w/o Creston Road | Arterial | 13,300 ADT | LOS A-B |
| Santa Ynez Avenue e/o Creston Road | Local | 950 ADT | LOS A-B |
| Via Ramona n/o Scott Street | Local | 260 ADT | LOS A-B |
| Commerce Way n/o Scott Street | Industrial | 4,300 ADT | LOS A-B |

All of the key roadways currently operate at LOS A-B. The roadway segment levels of service are provided in ranges (e.g. LOS A-B) because volumes and operations fluctuate throughout the day. A transportation system's ability to accommodate traffic is typically
measured during peak demand periods at intersections, as they are the major constraint in the system. Table 2 shows the operation of the key intersections during the A.M. and P.M. peak commuter periods. Levels of service for the intersections were calculated using the Highway Capacity Manual operations methodology. ${ }^{1}$ As shown, the signalized Creston Rd/Sherwood Rd-Niblick Rd intersection operates at LOS C during the morning and evening peak commuter periods, while the unsignalized intersections of Creston Rd/Santa Ynez Ave and Creston Rd/Scott St operate at LOS B during the peak commuter periods.

Table 2
Existing Intersection Operations

| Intersection | Control | Delay / LOS |  |
| :---: | :---: | :---: | :---: |
|  |  | A.M. Peak | P.M. Peak |
| Creston Rd/Sherwood Rd-Niblick Rd | Signal | $16.7 \mathrm{Sec} / \mathrm{LOS} \mathrm{C}$ | 18.5 Sec / LOS C |
| Creston Rd/Santa Ynez Ave | All-Way Stop | 8.1 Sec / LOS B | 6.7 Sec / LOS B |
| Creston Rd/Scott St | 1-Way Stop | $7.4 \mathrm{Sec} / \mathrm{LOS} \mathrm{B}$ | $7.8 \mathrm{Sec} / \mathrm{LOS} \mathrm{B}$ |

LOS based on average delay per vehicle.

## TRAFFIC DIVERSIONS

Figure 4 shows the traffic diversions that were modeled assuming that the first block of Scott Street were closed. The diversions were modeled based on the existing traffic patterns observed, which show that the diverted traffic is primarily oriented to/from the residential uses east of Commerce Way, and to a lesser degree the southern portions of Via Ramona, Camino Lobo and Commerce Way, as well as the northern portion of the Driftwood Drive neighborhood. The existing patterns also shows that about 70\% of the traffic is oriented to the north on Creston and $30 \%$ to the south on Creston. Most of the 3,050 ADT that currently uses the first block of Scott Street would divert to Commerce Way when entering and existing the neighborhood (1,700 ADT). 525 ADT are expected to enter and exit the neighborhood via Santa Ynez Avenue, with about 615 ADT are expected to use Cedarwood Drive. Most of the diversions on Santa Ynez Avenue and Cedarwood Drive are trips oriented to the south on Creston. About 200 ADT are expected to use Airport Road to enter and exit the eastern portion of the neighborhood and access uses to the south (e.g. Peterson Elementary School).

[^1]Table 3 shows the roadway levels of service assuming the street closure. Most of the key roadways are forecast to continue to operate at LOS A-B. Commerce Way would receive about 1,700 ADT and operate at LOS B-C. One of the issues that needs to be considered is the additional traffic on local residential streets. Santa Bella, Via Ramona, Camino Lobo and the north end of Driftwood Drive would receive some of the diverted traffic. These local street do, however, have ample capacity to accommodate the additional volumes.

## Table 3 <br> Roadway Operations with Scott Street Closed

| Roadway | Type | Volume | LOS |
| :--- | :---: | :---: | :---: |
| Scott Street w/o Creston Road | NA - Closed | NA - Closed | NA - Closed |
| Creston Road n/o Sherwood Road | Arterial | 14,500 ADT | LOS A-B |
| Creston Road s/o Sherwood Road | Arterial | 11,800 ADT | LOS A-B |
| Sherwood Road e/o Creston Road | Arterial | 10,200 ADT | LOS A-B |
| Niblick Road who Creston Road | Arterial | 13,300 ADT | LOS A-B |
| Santa Ynez Avenue e/o Creston Road | Local | 1,475 ADT | LOS A-B |
| Via Ramona n/o Scott Street | Local | 510 ADT | LOS A-B |
| Commerce Way n/o Scott Street | Industrial | 6,000 ADT | LOS B-C |

Table 4 shows that levels of service the key intersections would operate at LOS B or LOS C during the A.M. and P.M. peak commuter periods. These service levels would not change as a result of the street closure (compare to Table 2).

Table 4
Intersection Operations with Scott Street Closed

|  | Delay / LOS |  |  |
| :--- | :---: | :---: | :---: |
|  |  | Control | A.M. Peak |
| Preston Rd/Sherwood Rd-Niblick Rd | Signal | $16.9 \mathrm{Sec} / \mathrm{LOS} \mathrm{C}$ | $18.2 \mathrm{Sec} / \mathrm{LOS} \mathrm{C}$ |
| Creston Rd/Santa Ynez Ave | All-Way Stop | $7.3 \mathrm{Sec} / \mathrm{LOS} \mathrm{B}$ | $5.9 \mathrm{Sec} / \mathrm{LOS} \mathrm{B}$ |
| Creston Rd/Scott St | NA - Closed | NA - Closed | NA - Closed |

LOS based on average delay per vehicle.

## CIRCULATION ELEMENT CONSIDERATIONS

Although the effects of the diversions would not significantly change levels of service on the affected roadways and intersections, there must be some consideration of the City's future circulation needs in this area. The Circulation Element identifies Scott Street as a collector road (see Figure 5). Ultimately the roadway is to extend easterly and connect with a northsouth collector road (which is unnamed and unconstricted). Collector roads such as Scott Street are intended to move traffic between arterial and local streets as well as link neighborhoods and commercial uses. Closing the first block of Scott Street would withdraw some of Scott Street's intended use. If the City chooses to close the first block of Scott Street, parallel surface streets such as Linne Road and Meadowlark Road would have to carry the some of the future traffic generated to the east (see Figure 5). The alternate routes have the capacity to accommodate the relatively low volume of diverted trips without significantly changing levels of service.

Consideration was also given to providing a new roadway link between Scott Street and Cedarwood Drive in the vicinity of the street closure. The most logical place from a traffic flow standpoint, would be to extend the roadway link from the south end of Via Ramona across Oak Creek Park and connect with Cedarwood Drive at the north end of Beachwood. This link would carry about 800 to 1,200 ADT and serve as a local street, linking the neighborhood with the commercial uses adjacent to Creston/Cedarwood as well as providing additional access to Creston. However, much of the traffic diversion resulting from closing the first block of Scott Street is traffic oriented to and from the north via Creston. Thus, a link to the south would be expected to carry relatively low traffic volumes.


## RLP/DLD

attachments






Lanes, Volumes, Timings

| Lane Group | $\begin{gathered} \text { E } \\ E B L \end{gathered}$ | EBT | EBR | WBL | WBT | WBR | $\cdots$ | NBT | N昂 | S 4 | S $\downarrow$ | S |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  |  |  |  | ¢ |  | 170 |  |  | 3 | Af |  |
| Satd. Flow (prot) | 1770 | 1740 | 0 | 1770 | 1734 | 0 | 1770 | 3718 | 0 | 1770 | 3357 | 0 |
| Flt Perm. | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (perm) | 1770 | 1740 | 0 | 1770 | 1734 | 0 | 1770 | 3718 | 0 | 1770 | 3357 | 0 |
| - Volume (vph) | 97 | 137 | 106 | 22 | 147 | 126 | 288 | 342 | 5 | 109 | 155 | 302 |
| Lane Group Flow (vph) | 108 | 270 | 0 | 24 | 303 | 0 | 320 | 405 | 0 | 121 | 534 | 0 |
| Perm or Prot? | Prot |  |  | Prot |  |  | Prot |  |  | Prot |  |  |
| Phase Number | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Maximum Split (s) | 8 | 17 |  | 6 | 15 |  | 14 | 15 |  | 12 | 13 |  |
| Lost Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| g/c Ratio | 0.10 | 0.28 |  | 0.06 | 0.24 |  | 0.22 | 0.24 |  | 0.18 | 0.20 |  |
| Lane Grp Cap (vph) | 177 | 487 |  | 106 | 416 |  | 389 | 892 |  | 319 | 671 |  |
| V/C Ratio | 0.61 | 0.55 |  | 0.23 | 0.73 |  | 0.82 | 0.45 |  | 0.38 | 1.11dr |  |
| VIS Ratio Prot | 0.06 |  |  | 0.01 |  |  | 0.18 |  |  | 0.07 |  |  |
| V/S Ratio Perm |  | 0.16 |  |  | 0.17 |  |  | 0.11 |  |  | 0.16 |  |
| Critical LG? | Yes |  |  |  | Yes |  | Yes |  |  |  | Yes |  |
| Uniform Delay, d1 | 16.4 | 11.7 |  | 17.0 | 13.3 |  | 14.1 | 12.3 |  | 13.7 | 14.4 |  |
| Platoon Factor | 1.00 | 0.69 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incr. Delay, d2 | 4.2 | 1.1 |  | 0.2 | 4.3 |  | 9.1 | 0.3 |  | 0.4 | 4.6 |  |
| Webster's St Delay | 20.6 | 9.2 |  | 17.2 | 17.6 |  | 23.2 | 12.6 |  | 14.1 | 19.0 |  |
| LOS | C | B |  | C | C |  | C | B |  | B | C |  |

Cycle Length: 50
Control Type: Actuated-Coordinated
Lost Time: 12
Sum of Critical VIS Ratios: 0.58
Intersection VIC Ratio: 0.76
Intersection Webster Stopped Delay: 16.7
Intersection LOS: C
dr Defacto Right Lane. Recode with 1 though lane as a right lane.
Splits and Phases: Niblick \& Creston

| 51 |  |  | $\rightarrow 2$ |  |  | $4{ }_{7} 3$ |  |  | $\downarrow 14$ | E. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 |  |  | 17 |  |  | 14 |  |  | 13 |  | 50 |
| 8 | 8 | $5^{5}$ |  |  |  | 12 |  |  |  |  | 3xay |
|  | $\bigcirc$ |  |  |  |  | 47 |  | $\uparrow 8$ |  |  |  |

## Lanes, Volumes, Timings

| Lane Group |  | EBT | EBR | WBL | WBT |  | NBL | NT | $\cdots$ | S | S $\begin{array}{r}\text { ¢ } \\ \text { SBT }\end{array}$ | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  |  |  |  |  |  |  |  |  |  |  |  |
| Satd. Flow (prot) | 1770 | 1699 | 0 | 1770 | 1714 | 0 | 1770 | 3699 | 0 | 1770 | 3569 | 0 |
| FIt Perm. | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (perm) | 1770 | 1699 | 0 | 1770 | 1714 | 0 | 1770 | 3699 | 0 | 1770 | 3569 | 0 |
| Volume (vph) | 154 | 161 | 230 | 11 | 153 | 176 | 192 | 299 | 14 | 173 | 373 | 144 |
| Lane Group Flow (vph) | 171 | 435 | 0 | 12 | 366 | 0 | 213 | 366 | 0 | 192 | 603 | 0 |
| Perm or Prot? | Prot |  |  | Prot |  |  | Prot |  |  | Prot |  |  |
| Phase Number | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Maximum Split (s) | 10 | 23 |  | 6 | 19 |  | 12 | 12 |  | 14 | 14 |  |
| Lost Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| $\mathrm{g} / \mathrm{c}$ Ratio | 0.13 | 0.36 |  | 0.05 | 0.29 |  | 0.16 | 0.16 |  | 0.20 | 0.20 |  |
| Lane Grp Cap (vph) | 225 | 618 |  | 97 | 499 |  | 290 | 605 |  | 354 | 714 |  |
| V/C Ratio | 0.76 | 0.70 |  | 0.12 | 0.73 |  | 0.74 | 0.60 |  | - 0.54 | 0.84 |  |
| V/S Ratio Prot | 0.10 |  |  | 0.01 |  |  | 0.12 |  |  | 0.11 |  |  |
| V/S Ratio Perm |  | 0.26 |  |  | 0.21 |  |  | 0.10 |  |  | 0.17 |  |
| Critical LG? | Yes |  |  |  | Yes |  | Yes |  |  |  | Yes |  |
| Uniform Delay, d1 | 17.6 | 11.4 |  | 18.8 | 13.3 |  | 16.6 | 16.2 |  | 15.0 | 16.1 |  |
| Platoon Factor | 1.00 | 0.69 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incr. Delay, d2 | 9.3 | 2.5 |  | 0.0 | 3.8 |  | 6.4 | 1.2 |  | 1.3 | 6.4 |  |
| Webster's St Delay | 26.9 | 10.3 |  | 18.8 | 17.2 |  | 23.0 | 17.5 |  | 16.3 | 22.5 |  |
| LOS | D | B |  | C | C |  | C | C |  | C | C |  |

Cycle Length: 55
Control Type: Actuated-Coordinated
Lost Time: 12
Sum of Critical V/S Ratios: 0.60
Intersection VIC Ratio: 0.77
Intersection Webster Stopped Delay: 18.5
Intersection LOS:
Splits and Phases: Niblick \& Creston

| $\downarrow$ |  | $\rightarrow 2$ |  | $4{ }^{4} 13$ |  | $\downarrow{ }^{4}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 |  | 23 | $12 \times 5{ }^{1}$ |  |  | 14 |  |  |
| 10 |  | $\operatorname{han}^{2}$ |  | 14 |  | $1$ | 12 |  |
| $\bigcirc$ | 5 | $\leftarrow 6$ |  | 4 |  |  | $\uparrow$ |  |

Lanes, Volumes, Timings

| Lane Group | $\begin{gathered} \sigma \\ \text { EBL } \end{gathered}$ | $\begin{aligned} & \text { E } \\ & \text { EBT } \end{aligned}$ | $\begin{gathered} 7 \\ E B R \\ \hline \end{gathered}$ | WBL | $\underset{W B T}{\leftrightarrows}$ | $\begin{gathered} \boxed{Q} \\ \underline{W B R} \end{gathered}$ | $\underset{N B L}{N B}$ | NT ${ }^{\uparrow}$ | N | S | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | ${ }_{\text {H }}$ |  | 1 | t |  |  |  |  | $\frac{1}{1770}$ | ${ }_{\text {4t }}$ |  |
| Satd. Flow (prot) | 1770 | 1820 | 0 | 1770 | 1753 | 0 | 1770 | 3778 | 0 | 1770 | 3357 | 0 |
| Fit Perm. | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (perm) | 1770 | 1820 | 0 | 1770 | 1753 | 0 | 1770 | 3718 | 0 | 1770 | 3357 | 0 |
| Volume (vph) | 97 | 206 | 37 | 22 | 197 | 126 | 238 | 342 | 5 | 109 | 155 | 302 |
| Lane Group Flow (vph) | 108 | 270 | 0 | 24 | 359 | 0 | 264 | 405 | 0 | 121 | 534 | 0 |
| Perm or Prot? | Prot |  |  | Prot |  |  | Prot |  |  | Prot |  |  |
| Phase Number | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Maximum Split (s) | 8 | 17 |  | 6 | 15 |  | 14 | 15 |  | 12 | 13 |  |
| Lost Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| g/c Ratio | 0.10 | 0.28 |  | 0.06 | 0.24 |  | 0.22 | 0.24 |  | 0.18 | 0.20 |  |
| Lane Grp Cap (vph) | 177 | 510 |  | 106 | 421 |  | 389 | 892 |  | 319 | 671 |  |
| VIC Ratio | 0.61 | 0.53 |  | 0.23 | 0.85 |  | 0.68 | 0.45 |  | 0.38 | 1.11dr |  |
| VIS Ratio Prot | 0.06 |  |  | 0.01 |  |  | 0.15 |  |  | 0.07 |  |  |
| VIS Ratio Perm |  | 0.15 |  |  | 0.20 |  |  | 0.11 |  |  | 0.16 |  |
| Critical LG? | Yes |  |  |  | Yes |  | Yes |  |  |  | Yes |  |
| Uniform Delay, d1 | 16.4 | 11.5 |  | 17.0 | 13.8 |  | 13.6 | 12.3 |  | 13.7 | 14.4 |  |
| Platoon Factor | 1.00 | 0.70 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incr. Delay, d2 | 4.2 | 0.8 |  | 0.2 | 10.8 |  | 3.2 | 0.3 |  | 0.4 | 4.6 |  |
| Webster's St Delay | 20.6 | 8.9 |  | 17.2 | 24.6 |  | 16.8 | 12.6 |  | 14.1 | 19.0 |  |
| LOS | C | B |  | C | C |  | C | B |  | B | C |  |

Cycle Length: 50
Control Type: Actuated-Coordinated Lost Time: 12
Sum of Critical V/S Ratios: 0.57
Intersection V/C Ratio: 0.76
Intersection Webster Stopped Delay: 16.9
Intersection LOS: C
dr Defacto Right Lane. Recode with 1 though lane as a right lane.
Splits and Phases: Niblick \& Creston

| $\checkmark$ |  |  |  | $\rightarrow 2$ |  | - | $4{ }_{4} 3$ | $\downarrow / 4$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6 |  |  | 17 |  |  | 14 |  |  | 13 |  | 5asity |
|  | 8 |  |  | $5$ |  |  | 12 |  |  |  |  |  |
|  | $\bigcirc$ | 5 |  | 4 | $\leftarrow$ |  | 47 |  | $\uparrow 8$ |  |  |  |

## Lanes, Volumes, Timings

| Lane Group | $\begin{gathered} E=B \\ E B L \end{gathered}$ | $\underset{~ E}{\rightarrow}$ | EBR |  | WBT | WBR | N ${ }_{\text {昂 }}$ |  |  | S $\square_{\text {BL }}$ | S ${ }_{\text {d }}$ | S |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations Satd. Flow (prot) |  |  | 0 | $\frac{1}{1770}$ | $\stackrel{\text { F }}{+1727}$ | 0 | 1770 170 | $\begin{aligned} & 44 \\ & 3599 \end{aligned}$ | 0 | $\frac{7}{1770}$ | $41$ $3569$ | 0 |
| Flt Perm. | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (perm) | 1770 | 1727 | 0 | 1770 | 1727 | 0 | 1770 | 3699 | 0 | 1770 | 3569 | 0 |
| Volume (vph) | 154 | 205 | 196 | 11 | 187 | 176 | 158 | 299 | 14 | 173 | 373 | 144 |
| Lane Group Flow (vph) | 171 | 446 | 0 | 12 | 404 | 0 | 176 | 366 | 0 | 192 | 603 | 0 |
| Perm or Prot? | Prot |  |  | Prot |  |  | Prot |  |  | Prot |  |  |
| Phase Number | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Maximum Split (s) | 10 | 24 |  | 6 | 20 |  | 11 | 12 |  | 13 | 14 |  |
| Lost Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| g/c Ratio | 0.13 | 0.38 |  | 0.05 | 0.31 |  | 0.15 | 0.16 |  | 0.18 | 0.20 |  |
| Lane Grp Cap (vph) | 225 | 659 |  | 97 | 534 |  | 257 | 605 |  | 322 | 714 |  |
| V/C Ratio | 0.76 | 0.68 |  | 0.12 | 0.76 |  | 0.68 | 0.60 |  | -0.60 | 0.84 |  |
| V/S Ratio Prot | 0.10 |  |  | 0.01 |  |  | 0.10 |  |  | 0.11 |  |  |
| VIS Ratio Perm |  | 0.26 |  |  | 0.23 |  |  | 0.10 |  |  | 0.17 |  |
| Critical LG? | Yes |  |  |  | Yes |  | Yes |  |  |  | Yes |  |
| Uniform Delay, d1 | 17.6 | 10.8 |  | 18.8 | 13.0 |  | 16.9 | 16.2 |  | 15.7 | 16.1 |  |
| Platoon Factor | 1.00 | 0.68 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incr. Delay, d2 | 9.3 | 1.9 |  | 0.0 | 4.2 |  | 4.9 | 1.2 |  | 2.2 | 6.4 |  |
| Webster's St Delay | 26.9 | 9.2 |  | 18.8 | 17.3 |  | 21.9 | 17.5 |  | 17.8 | 22.5 |  |
| LOS | D | B |  | C | C |  | C | C |  | C | C |  |

Cycle Length: 55
l Control Type: Actuated-Coordinated Lost Time: 12
Sum of Critical V/S Ratios: 0.60
Intersection VIC Ratio: 0.77
Intersection Webster Stopped Delay: 18.2
Intersection LOS: C
Splits and Phases: Niblick \& Creston



Intersection Performance Summary

University of Florida
512 Weil Hall
$3^{-\prime}$ nesville, FL 32611-2083
i (904) 392-0378

Streets: (N-S) CRESTON (E-W) SANTA YNEZ
Mnalyst..................... D D D
Jate of Analysis.......... 3/9/99
Jther Information......... EXISTING PM PEAK
All-way Stop-controlled Intersection


Volume Summary and Capacity Analysis WorkSheet

|  | NB | SB | EB | WB |
| :---: | :---: | :---: | :---: | :---: |
| T Flow Rate | 0 | 26 |  | 8 |
| :T Flow Rate | 8 | 0 |  | 17 |
| spproach Flow Rate | 536 | 657 |  | 25 |
| roportion LT | 0.00 | 0.04 |  | 0.32 |
| 'roportion RT | 0.01 | 0.00 |  | 0.68 |
| pposing Approach Flow Rate | 657 | 536 |  | 0 |
| :onflicting Approaches Flow Rate | 25 | 25 |  | 1193 |
| 'roportion, Subject Approach Flow Rate | 0.44 | 0.54 |  | 0.02 |
| roportion, Opposing Approach Flow Rate | 0.54 | 0.44 |  | 0.00 |
| - : on Subject Approach | 2 | 3 |  | 2 |
| - on Opposing Approach | 3 | 2 |  | 0 |
| T, Opposing Approach | 26 | 0 |  | 0 |
| T, Opposing Approach | 0 | 8 |  | 0 |
| T, Conflicting Approaches | 8 | 8 |  | 26 |
| T, Conflicting Approaches | 17 | 17 |  | 8 |
| roportion LT, Opposing Approach | 0.04 | 0.00 |  | 0.00 |
| roportion RT, Opposing Approach | 0.00 | 0.01 |  | 0.00 |
| roportion LT, Conflicting Approaches | 0.32 | 0.32 |  | 0.02 |
| roportion RT, Conflicting Approaches | 0.68 | 0.68 |  | 0.01 |
| pproach Capacity | 1014 | 1358 |  | 416 |

Intersection Performance Summary

| Yovement | Approach Flow Rate | Approach Capacity | $\begin{gathered} \text { v/C } \\ \text { Ratio } \end{gathered}$ | Average <br> Total Delay | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NB | 536 | 1014 | 0.53 | 7.5 | B |
| SB | 657 | 1358 | 0.48 | 6.3 | B |
| WB | 25 | 416 | 0.06 | 1.3 | A |
|  | Intersection Delay $=6.7$ <br> Level of Service (Intersection) $=B$ |  |  |  |  |



Intersection Performance Summary

| Movement | Approach Flow Rate | Approach Capacity | $\begin{gathered} \text { V/C } \\ \text { Ratio } \end{gathered}$ | Average Total Delay | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NB | 592 | 967 | 0.61 | 10.2 | C |
| SB | 240 | 1202 | 0.20 | 2.1 | A |
| WB | 85 | 488 | 0.17 | 1.9 | A |
|  | Intersection Delay $=7.3$ <br> Level of Service (Intersection) $=B$ |  |  |  |  |



Intersection Performance Summary

| Movement | Approach Flow Rate | Approach Capacity | $\begin{gathered} \text { V/C } \\ \text { Ratio } \end{gathered}$ | Average Total Delay | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NB | 493 | 991 | 0.50 | 6.6 | B |
| SB | 608 | 1346 | 0.45 | 5.6 | B |
| WB | 40 | 428 | 0.09 | 1.4 | A |
|  | Intersection Delay $=5.9$ Level of Service (Intersection) $=B$ |  |  |  |  |

Canter For Mioromplpters In Irarsportation University of Florich
512 Heil Hall
Gairesville, f. 3811-2063
Ph: ( 504 ) $3 \times 2-0578$

HSS: Unsignalized Intersactiars Release 2.1f BAMG.HD Page 2
Ubrksheet for MSC Intersection





| O\%「 | $0^{\circ}$ | prod sou! unl 7737 |
| :---: | :---: | :---: |
| OE\& | $05^{*} 9$ | pray nutw כ!ffer ¢parl |
| $00^{\circ} \mathrm{C}$ | $0 S^{\circ} \mathrm{S}$ | proy Jatw unl |
| 0172 | $0 S^{\circ} \mathrm{S}$ |  |
| (H) Hul | (4) dty | cmath |
| CWroly | ¢ | эЈ! |
|  | s.oqx |  |




Hans



 ITOIS Ш1 W ( $4-3$ ) Nisem (S-N) :spons


eploly fo kissorlun

2 obed CaH"ghtel th"



[^0]:    Attachments: Exhibit A - Sherwood/Oak Creek Park Master Plan Exhibit B - Senior Center \& Veteran's War Memorial Building Concept Exhibit C - Traffic Study re: Partial Closure of Scott Street

[^1]:    1 Highway Capacity Manual, Special Report 209, Transportation Research Board, National Research Council, Washington, D.C. 1994.

